

3.1.7 *cdf*—the cumulative distribution function (cdf), denoted by $F(t)$, represents the probability of failure (or the population fraction failing) by time = (t) . See section 3.1.4.

3.1.8 *Weibull distribution*—For the purposes of this guide, the Weibull distribution is represented by the equation:

$$F(t) = 1 - e^{-\left(\frac{t}{c}\right)^b} \quad (2)$$

where:

- $F(t)$ = defined in paragraph 3.1.4
- t = units of time used for service life
- c = scale parameter
- b = shape parameter

3.1.8.1 The shape parameter (b), section 3.1.6, is so called because this parameter determines the overall shape of the curve. Examples of the effect of this parameter on the distribution curve are shown in Fig. 1, section 5.3.

3.1.8.2 The scale parameter (c), section 3.1.6, is so called because it positions the distribution along the scale of the time axis. It is equal to the time for 63.2 % failure.

NOTE 1—This is arrived at by allowing t to equal c in the above expression. This then reduces to Failure Probability = $1 - e^{-1}$, which further reduces to equal $1 - 0.368$ or $.632$.

3.1.9 *complete data*—A complete data set is one where all of the specimens placed on test fail by the end of the allocated test time.

3.1.10 *Incomplete data*—An incomplete data set is one where (a) there are some specimens that are still surviving at the expiration of the allowed test time, (b) where one or more specimens is removed from the test prior to expiration of the allowed test time. The shape and scale parameters of the above distributions may be estimated even if some of the test specimens did not fail. There are three distinct cases where this might occur.

3.1.10.1 *Time censored*—Specimens that were still surviving when the test was terminated after elapse of a set time are

considered to be time censored. This is also referred to as right censored or type I censoring. Graphical solutions can still be used for parameter estimation. At least ten observed failures should be used for estimating parameters (for example slope and intercept).

3.1.10.2 *specimen censored*—Specimens that were still surviving when the test was terminated after a set number of failures are considered to be specimen censored. This is another case of right censored or type I censoring. See 3.1.10.1

3.1.10.3 *Multiply Censored*—Specimens that were removed prior to the end of the test without failing are referred to as left censored or type II censored. Examples would include specimens that were lost, dropped, mishandled, damaged or broken due to stresses not part of the test. Adjustments of failure order can be made for those specimens actually failed.

4. Significance and Use

4.1 Service life test data often show different distribution shapes than many other types of data. This is due to the effects of measurement error (typically normally distributed), combined with those unique effects which skew service life data towards early failure (infant mortality failures) or late failure times (aging or wear-out failures) Applications of the principles in this guide can be helpful in allowing investigators to interpret such data.

NOTE 2—Service life or reliability data analysis packages are becoming more readily available in standard or common computer software packages. This puts data reduction and analyses more readily into the hands of a growing number of investigators.

5. Data Analysis

5.1 In the determinations of service life, a variety of factors act to produce deviations from the expected values. These factors may be of a purely random nature and act to either increase or decrease service life depending on the magnitude of the factor. The purity of a lubricant is an example of one such

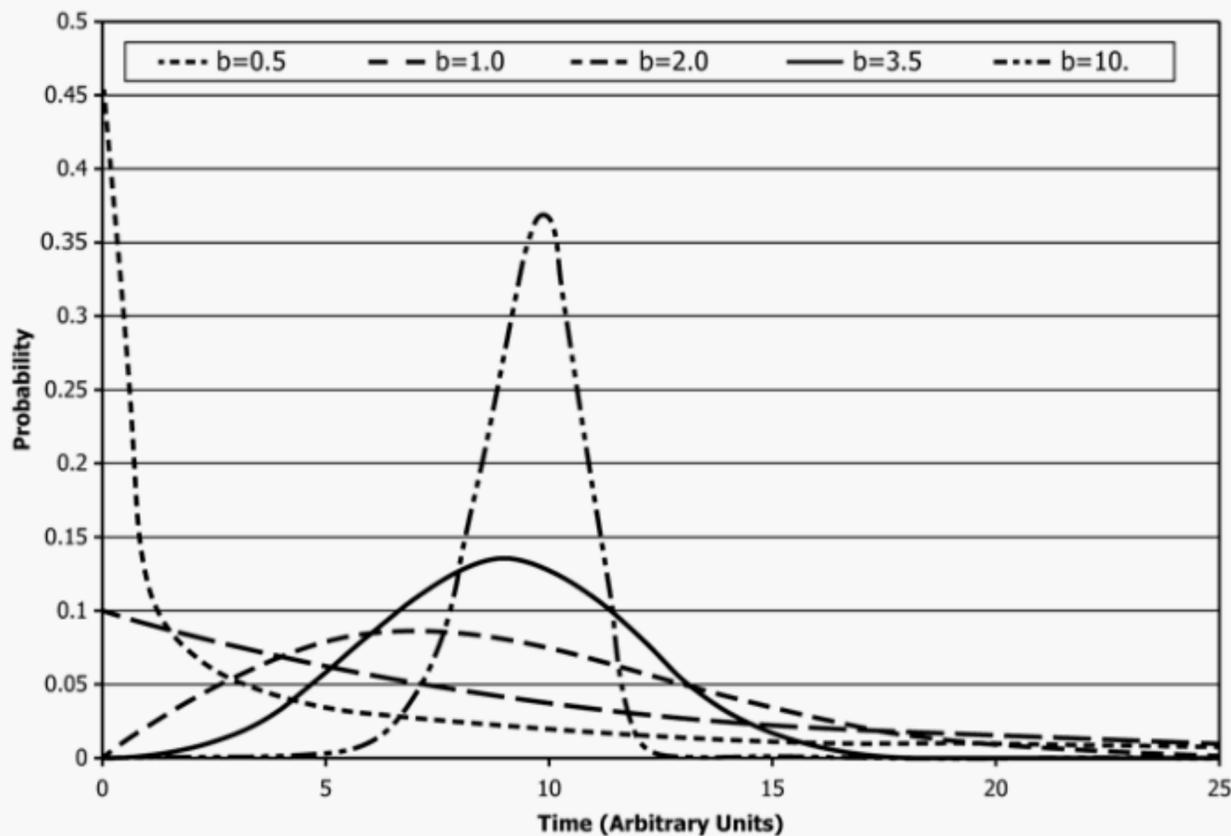


FIG. 1 Effect of the Shape Parameter (b) on the Weibull Probability Density

factor. An oil clean and free of abrasives and corrosive materials would be expected to prolong the service life of a moving part subject to wear. A fouled contaminated oil might prove to be harmful and thereby shorten service life. Purely random variation in an aging factor that can either help or harm a service life might lead a normal, or gaussian, distribution. Such distributions are symmetrical about a central tendency, usually the mean.

5.1.1 Some non-random factors act to skew service life distributions. Defects are generally thought of as factors that can only decrease service life. Thin spots in protective coatings, nicks in extruded wires, chemical contamination in thin metallic films are examples of such defects that can cause an overall failure even through the bulk of the material is far from failure. These factors skew the service life distribution towards early failure times.

5.1.2 Factors that skew service life towards the high side also exist. Preventive maintenance, high quality raw materials, reduced impurities, and inhibitors or other additives are such factors. These factors produce life time distributions shifted towards the long term and are those typically found in products having been produced a relatively long period of time.

5.1.3 Establishing a description of the distribution of frequency (or probability) of failure versus time in service is the objective of this guide. Determination of the shape of this distribution as well as its position along the time scale axis are the principle criteria for estimating service life.

5.2 *Normal (Gaussian) Distribution*—The characteristic of the normal, or Gaussian distribution is a symmetrical bell shaped curve centered on the mean of this distribution. The mean represents the time for 50 % failure. This may be defined as either the time when one can expect 50 % of the entire population to fail or the probability of an individual item to fail. The “scale” of the normal curve is the mean value (\bar{x}), and the shape of this curve is established by the standard deviation value (σ).

5.2.1 The normal distribution has found widespread use in describing many naturally occurring distributions. Its first known description by Carl Gauss showed its applicability to measurement error. Its applications are widely known and numerous texts produce exhaustive tables and descriptions of this function.

5.2.2 Widespread use should not be confused with justification for its application to service life data. Use of analysis techniques developed for normal distribution on data distributed in a non-normal manner can lead to grossly erroneous conclusions. As described in Section 5, many service life distributions are skewed towards either early life or late life. The confinement to a symmetrical shape is the principal shortcoming of the normal distribution for service life applications. This may lead to situations where even negative lifetimes are predicted.

5.3 *Lognormal Distribution*—This distribution has shown application when the specimen fails due to a multiplicative process that degrades performance over time. Metal fatigue is one example. Degradation is a function of the amount of

flexing, cracks, crack angle, number of flexes, etc. Performance eventually degrades to the defined end of life.³

5.3.1 There are several convenient features of the lognormal distribution. First, there is essentially no new mathematics to introduce into the analysis of this distribution beyond those of the normal distribution. A simple logarithmic transformation of data converts lognormal distributed data into a normal distribution. All of the tables, graphs, analysis routines etc. may then be used to describe the transformed function. One note of caution is that the shape parameter σ is symmetrical in its logarithmic form and non-symmetrical in its natural form. (For example, $\bar{x} = 1 \pm .2\sigma$ in logarithmic form translates to 10 +5.8 and -3.7 in natural form.)

5.3.2 As there is no symmetrical restriction, the shape of this function may be a better fit than the normal distribution for the service life distributions of the material being investigated.

5.4 *Weibull Distribution*—While the Swedish Professor Waloddi Weibull was not the first to use this expression,⁴ his paper, A Statistical Distribution of Wide Applicability published in 1951 did much to draw attention to this exponential function. The simplicity of formula given in (1), hides its extreme flexibility to model service life distributions.

5.4.1 The Weibull distribution owes its flexibility to the “shape” parameter. The shape of this distribution is dependent on the value of b . If b is less than 1, the Weibull distribution models failure times having a decreasing failure rate. The times between failures increase with exposure time. If $b = 1$, then the Weibull models failure times having constant failure rate. If $b > 1$ it models failure times having an increasing failure rate, if $b = 2$, then Weibull exactly duplicates the Rayleigh distribution, as b approaches 2.5 it very closely approximates the lognormal distribution, as b approaches 3. the Weibull expression models the normal distribution and as b grows beyond 4, the Weibull expression models distributions skewed towards long failure times. See Fig. 1 for examples of distributions with different shape parameters.

5.4.2 The Weibull distribution is most appropriate when there are many possible sites where failure might occur and the system fails upon the occurrence of the first site failure. An example commonly used for this type of situation is a chain failing when only one link separates. All of the sites, or links, are equally at risk, yet one is all that is required for total failure.

5.5 *Exponential Distribution*—This distribution is a special case of the Weibull. It is useful to simplify calculations involving periods of service life that are subject to random failures. These would include random defects but not include wear-out or burn-in periods.

6. Parameter Estimation

6.1 Weibull data analysis functions are not uncommon but not yet found on all data analysis packages. Fortunately, the expression is simple enough so that parameter estimation may

³ Mann, N. R. et al., *Methods for Statistical Analysis of Reliability and Life Data*, Wiley, New York 1974 and Gnedenko, B.V. et al, *Mathematical Methods of Reliability Theory*, Academic Press, New York 1969.

⁴ Weibull, W., “A statistical distribution of wide applicability,” *J. Appl. Mech.*, 18, 1951, pp 293–297.

be made easily. What follows is a step-by-step example for estimating the Weibull distribution parameters from experimental data.

6.1.1 The Weibull distribution, (Eq 2) may be rearranged as shown below: (Eq 3)

$$1 - F(t) = e^{-\left(\frac{t}{c}\right)^b} \quad (3)$$

and, by taking the natural logarithm of both sides twice, this expression becomes

$$\ln\left[\ln\frac{1}{1 - F(t)}\right] = b\ln(t) - b\ln(c) \quad (4)$$

Eq 4 is in the form of an equation describing a straight line ($y = mx + y_0$) with

$$\ln\left[\ln\frac{1}{1 - F(t)}\right] \quad (5)$$

corresponding to Y , $\ln(t)$ corresponding to x and the slope of the line m equals the Weibull shape parameter b . Time to failure, t , is the independent variable and is defined as the time at which some measurable performance parameter falls below a pre-defined critical value.

6.1.2 The failure probability, $F(t)$, associated with each failure time can be estimated using the median rank estimate approximation shown below:

$$F(t) = \frac{j - 0.3}{n + 0.4} \quad (6)$$

where:

j = the failure order and

n = the total number of specimens on test.

See Tobias and Trindade, section 2.2 and Johnson, section 3.1.3

7. Service Life Estimation

7.1 Select the distribution model that best fits the observed service life data. Often a simple graph will help not only in choosing a model but in detecting outlier data. Further guidance in selecting a distribution model can be obtained from linear regression coefficients of lifetime versus probability. Higher regression coefficients are an indication of a better model fit.

7.1.1 Neither the Weibull distribution nor any other distribution is a universal best choice for every situation or data set. Each data set must be checked and the best fitting model distribution selected for estimation purposes. See section 1.5.

7.2 Determine the shape and scale parameters of the distribution. A minimum of 10 failures is required to properly determine a distribution. The more the better, but there is a point of diminishing returns. A reasonable range of failed specimens is 10 to 50.

7.3 Calculate the probability of failure by a given time t or alternatively, the time to reach a given failure probability. See Example Calculations, section 8, for a step-by-step procedure for this calculation.

8. Example Calculations

8.1 Simple case - complete data set.

8.1.1 Consider a hypothetical case where 20 incandescent lamps are put on test. The lamps are labeled “A” through “T” at the beginning of the test. Each lamp was found to operate satisfactorily at the beginning of the test period. The lamps were all left on and inspected each day to determine if they were still burning. A data sheet was kept and the number of days of operation for each of the 20 lamps was recorded. The results are reported in Table 1.

8.1.2 The failure times were sorted from earliest (78 days) to latest (818 days) and the median rank, $F(t)$, calculated for each lamp. When the median rank has been calculated for each specimen, all of the information will be available that is needed to solve the Weibull expression:

$$1 - F(t) = e^{-\left(\frac{t}{c}\right)^b} \quad (7)$$

8.1.3 Step by step example:

8.1.4 First, calculate $F(t)$ from Eq 6, where j is the failure order and n is the total number of specimens on test. For the first failure $j = 1$ and n , the number of lamps used in this test, is 20. Therefore

$$F(t) = \frac{j - 0.3}{n + 0.4} \quad (8)$$

$$= \frac{1 - 0.3}{20 + 0.4}$$

$$= 0.034$$

Continuing this operation for all 20 failure times produces Table 2.

8.1.5 Next, substitute the values for $F(t)$ and t into Eq 4. The value for the first failure is shown below.

$$\ln\left[\ln\frac{1}{1 - 0.034}\right] = 3.355 \quad (9)$$

$$- 3.355 = b[\ln(78)] - b[\ln(c)].$$

8.1.6 Repeating this procedure for the remaining 19 lamps produces a total of 20 such equations. A simple linear regression may now be used to determine the critical parameters b and c .

The resulting regression equation produces the following:

$$Y = 1.62\ln(t) - 9.46 \quad (10)$$

8.1.7 The value for the slope, 1.62, is equal to the Weibull shape parameter. The scale parameter, c , can be determined by the expression:

TABLE 1 Time to Failure (days of operation) for Incandescent Lamps

Lamp ID	Days of Operation	Lamp ID	Days of Operation
A	293	K	189
B	282	L	818
C	535	M	114
D	421	N	550
E	710	O	80
F	166	P	191
G	208	Q	402
H	155	R	210
I	456	S	101
J	203	T	78

TABLE 2 Median Rank for Incandescent Lamps

Failure Order	Life(Days)	Median Rank F(t)	Failure Order	Life(Days)	Median Rank F(t)
1	78	0.034	11	210	0.525
2	80	0.083	12	282	0.574
3	101	0.132	13	293	0.623
4	114	0.181	14	402	0.672
5	155	0.230	15	421	0.721
6	166	0.279	16	456	0.770
7	189	0.328	17	535	0.819
8	191	0.377	18	550	0.868
9	203	0.426	19	710	0.917
10	208	0.475	20	818	0.966

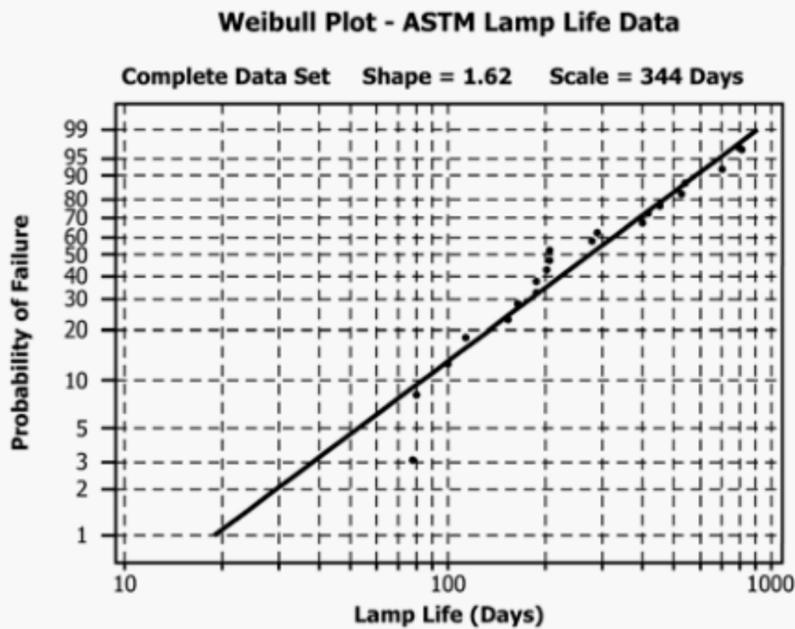


FIG. 2 Percent Probability of Failure Versus Time for Example Data

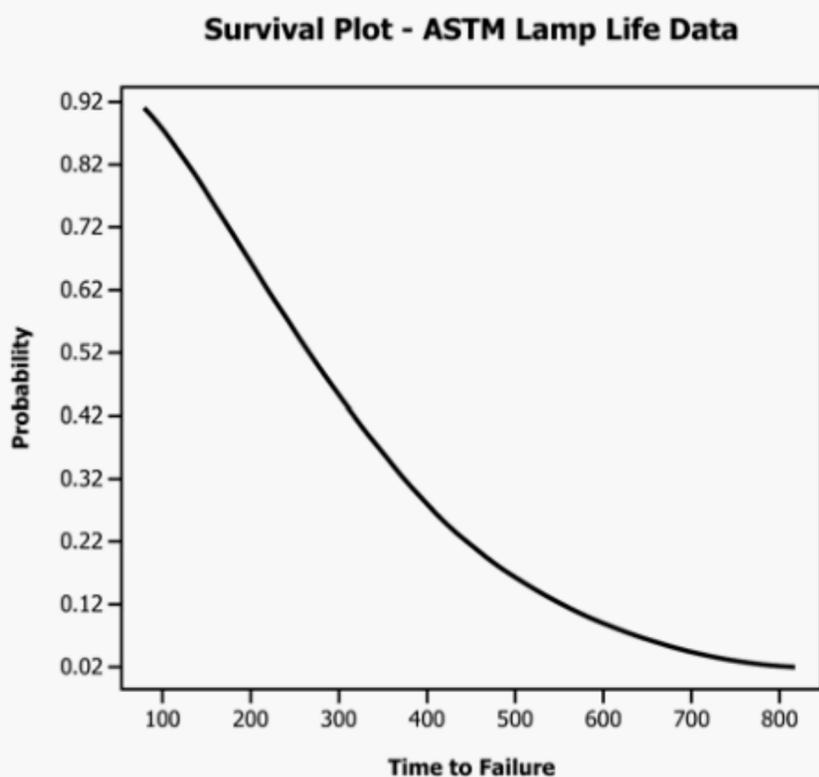


FIG. 3 Probability of Survival Plot for Example Data

$$c = \exp\left(\frac{-y_0}{b}\right) = 344 \text{ days} \quad (11)$$

8.1.8 Substituting the values of shape and scale into the Weibull expression (1) allows an accurate estimate of failure probability at any time (t).

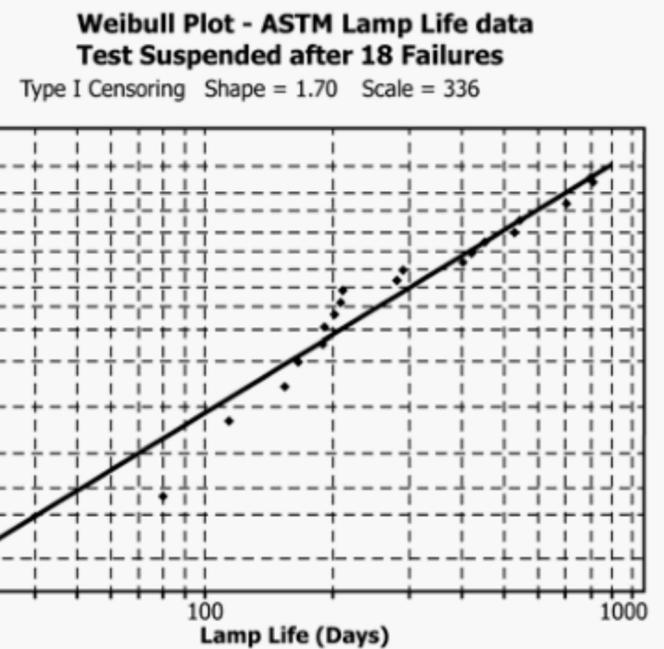


FIG. 4 Percent Probability of Failure Versus Time for Type I Censored Data

8.1.9 Graphical solutions to Weibull data are commonly made using paper specially scaled for the Weibull equation.⁵

8.1.10 The time to failure is plotted on a log scale and the probability of failure is plotted on a Weibull Scale. Such a plot is shown in Fig. 2.

As the probability of surviving, $R_{(t)}$, is simply $1-F_{(t)}$, then a probability of survival graph could also be made. It is customary to plot this in ordinary Cartesian coordinates with survival probability on the y axis and time on the x axis. The probability of survival graph for the above Weibull equation is shown in Fig. 3. This type of graph will be referred to as a Survival Plot.

8.2 Incomplete Data - Type I Censoring

8.2.1 There are various reasons that a test may be interrupted before all of the test specimens have failed. Using the analysis approach shown above, useful results may be obtained prior to the failure of the last specimens.

8.2.2 For this example, assume that the test was terminated after 18 months (considered here to be 550 days). Of the 20 specimens put on test, 18 had failed by that time. It was decided that sufficient failures had been obtained to reach a reasonable service life estimate.

8.2.3 The data analysis for this case is exactly the same as the example in section 8.1. The failure probability is calculated exactly the same, still using $n=20$ as the number of test specimens. After the 18 months have elapsed, the failure times versus median rank are regressed according to the Weibull equation.

8.2.4 The regression equation using this data set was found to be:

$$Y = 1.70 \ln(t) - 9.89 \quad (12)$$

8.2.5 The new shape parameter estimate is 1.70 and the new scale parameter estimate is 336 days. As can be seen, there is a good agreement between the parameters using the censored data and the complete data set. This data analysis is shown graphically in Fig. 4.

⁵ Nelson, W., and Thomson, V. C., "Weibull Probability Papers," *Journal of Quality Technology*, Vol. 3, No. 3, 1971, pp 45-50.

8.2.6 The corresponding survival plot for this data set is shown in Fig. 5

8.3 Incomplete Data - Type II Censoring:

8.3.1 Should a test specimen be removed from a test without having failed, and before the test is complete, that specimen is said to be Type II censored (also known as left censored).

8.3.2 For this example, we will consider the same data set but assume that on the 421st day, lamp D was found to have been broken by accidental contact. The lamp had been operating when checked earlier that day. All that can be said regarding the failure order for this lamp is that it could have been the 15th, 16th, 17th, 18th, 19th or the 20th failure.

8.3.3 There is now a degree of uncertainty regarding the failure order of the remaining 5 lamps. When lamp I fails on the 456th day, it could have been the 15th or the 16th failure depending on if lamp D would have failed before or after lamp I. A similar uncertainty exists about the remaining unfailed lamps.

8.3.4 Accounting for this uncertainty requires a small adjustment to reflect the probability of failure order. This adjustment is shown in the equation below.

$$i_j = \frac{(n+1) - O_p}{1 + n_r} \tag{13}$$

where:

- i = The increment for the j th failure
- n = Total number of specimens
- O_p = Failure Order of the Previous failure
- n_r = Total number of remaining specimens including the current one.

8.3.5 For specimen I it was known that the failure order before I was 14 (O_p). Also, there are 5 specimens (including I) to yet have failure orders assigned. The total number of specimens remains at 20. Therefore, for specimen I, the failure order increment is

$$i_j = \frac{(20+1) - 14}{1+5} = 1.167 \tag{14}$$

The failure order for specimen I is 14 + 1.167 or 15.167.

8.3.6 For the next specimen to fail after I, (specimen C) the calculation is repeated.

$$i_j = \frac{(n+1) - 15.167}{1+4} = 1.167 \tag{15}$$

Therefore the failure order for specimen C is 15.167 + 1.167 or 16.334.

8.3.7 If we again terminate our test after 18 months making specimen N the last failure observed, its failure order increment is also 1.167 giving it a failure order of 17.50

8.3.8 Performing the regression with this data set containing 17 failed specimens, 1 specimen type II censored and 2 specimens type I censored produces the following expression:

$$y = 1.68 \ln(t) - 9.76 \tag{16}$$

This indicates a shape of 1.68 and a scale of 333 days.

8.3.9 A graph of this data is shown in Fig. 6:

8.4 Comparison of Estimates for shape and Scale Parameters

8.4.1 A summary of three estimates obtained in this guide is shown in Table 3.

It may be seen that there is excellent agreement among these estimates.

9. Lifetime Estimates

9.1 Once the shape and scale parameters for the Weibull distribution have been determined, the equation can be used for life time estimates. Substitution of the shape and scale parameters into the Weibull calculation allows one to readily calculate the percent failure at any given time (t) or conversely, to calculate the time at which a certain percent failure will occur. This is permitted over a wide range of service life distributions and estimates may be made with complete or incomplete data.

9.2 Percent Failure at a given time.

9.2.1 As an example of this calculation, assume that one wanted to establish a warranty period of 180 days. Substituting into the Weibull equation:

$$1 - F(t) = e^{-\left(\frac{t}{c}\right)^b} \tag{17}$$

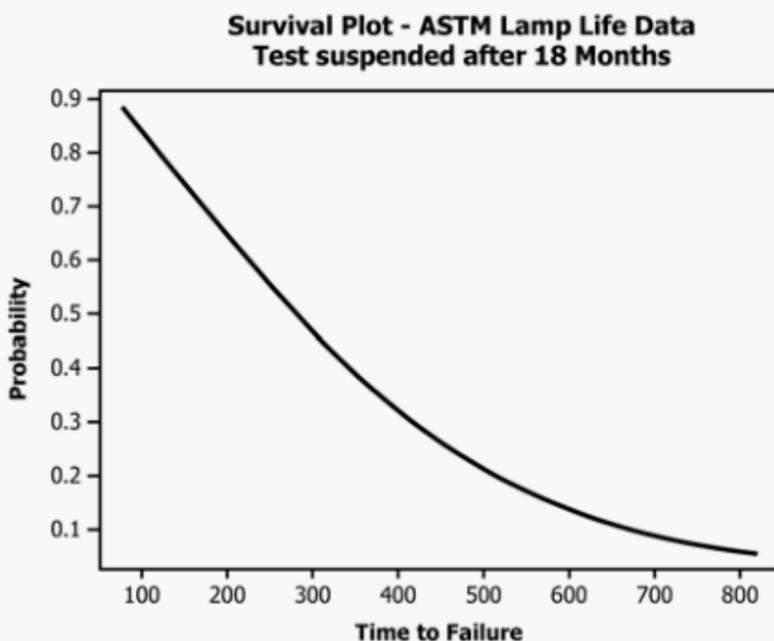


FIG. 5 Probability of Survival Versus Time for Type I Censored Data

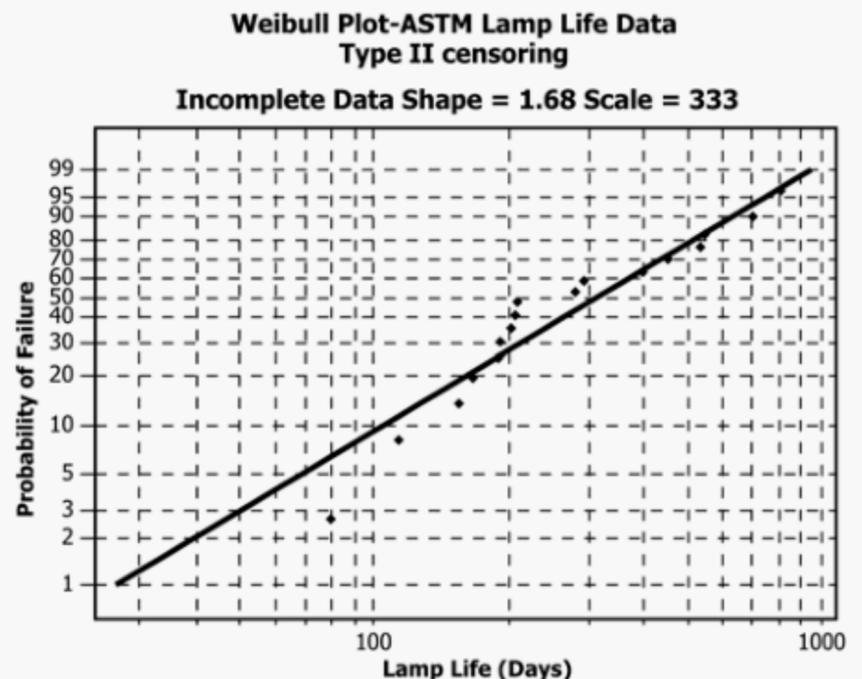


FIG. 6 Percent Probability of Failure Versus Time for Multiply Censored Data The Survival Plot is Also Shown:

Survival Plot - ASTM Lamp Life Data
Lamp D - Type II Censored at 421 Days
Test suspended after 18 Months

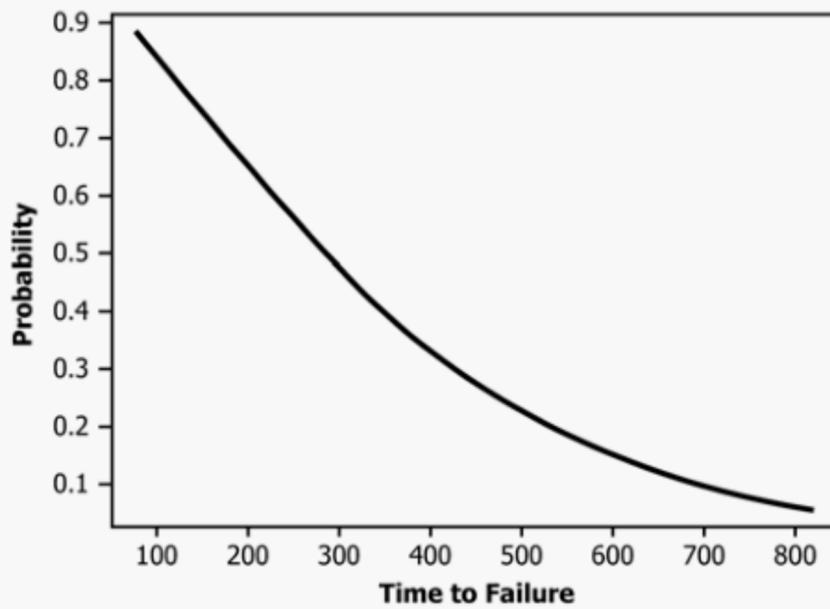


FIG. 7 Probability of Survival Versus Time for Type I Censored Data

TABLE 3 Comparison of Weibull Parameters From Example Data Treatments

Example	Shape	Scale
Complete Data set	1.62	344
Type I Censored	1.70	336
Type II Censored	1.68	333

and using the values from the complete data set (section 8.1), we have of 1.62 for shape (b), and 344 days for scale(c). The time (t) for evaluation is 180 days. Substituting into the equation produces:

$$1 - F(t) = e^{-\left(\frac{180}{344}\right)^{1.62}} \quad (18)$$

which equals

$$1 - F(t) = e^{-(0.5233)^{1.62}} \quad (19)$$

$$1 - F(t) = e^{-0.3502}$$

$$1 - F(t) = .705$$

$$F(t) = .295 \text{ or } 29.5\%$$

This indicates that 29.5 percent of the lamps would be expected to fail within the first 180 days. This value is in good agreement with the graphical solution shown in Fig. 2.

9.3 If one wanted to find the time for 10 percent failure, use the same equation but now rearrange as shown in Eq 20

$$\ln\left[\ln\frac{1}{1 - F(t)}\right] = b\ln(t) - b\ln c \quad (20)$$

9.3.1 Substitution 0.10 as the fraction for 10 % into this equation for F(t), and again using the shape and scale values from the complete data set, the equation becomes:

$$\ln\left[\ln\frac{1}{1 - .10}\right] = 1.62\ln(t) - 1.62\ln 344 \quad (21)$$

$$\ln[\ln(1.111)] = 1.62\ln(t) - 1.62\ln 344$$

$$\ln[.1053] = 1.62\ln(t) - 1.62(5.841)$$

$$\frac{-2.2509}{1.62} = \ln(t) - 5.841$$

$$-1.389 = \ln(t) - 5.841$$

$$4.452 = \ln(t)$$

$$t = e^{4.452} = 86 \text{ days}$$

This is also in good agreement with the graphical solution shown in the Fig. 1.

10. Summary

10.1 This guide has shown how to calculate the Weibull shape and scale parameters from experimental data. This has been shown in detail for situations where all of the specimens have failed, (complete data set), where the test is terminated before all of the specimens have failed (Type I censoring) and where some of the specimens have been removed from test without failure (Type II censoring).

10.2 It has also been shown in detail, how to utilize the Weibull equation to calculate the percentage of failures that can be expected to occur by a given time and also the time expected for a given percentage to fail.

10.3 The Weibull distribution can be used for further analysis, such as comparison of product service life at given times. This method can also be used on samples stressed at accelerated conditions as well as normal conditions. This makes it a key element in estimating service life at usage conditions from data collected at accelerated conditions.

REFERENCES

- (1) Nelson, W., *Accelerated Testing*, New York, John Wiley and Sons; 1990
- (2) Meeker, W. Q., and Escobar, L.A., *Statistical Methods for Reliability Data*, New York, John Wiley and Sons, 1998
- (3) Paul A. Tobias and David Trindade, *Applied reliability*, New York, Van Norstrand Reinhold, 1986
- (4) James A. McLinn, "Weibull Analysis Primer," 3rd edition, the Reliability Division of ASQC by Williams Enterprises, 1997
- (5) Johnson, Leonard G., *The Median Ranks of Sample values in their Population with an application to Certain Fatigue Studies*, Industrial Mathematics, Vol 2, 1 – 9, 1951.

ASTM International takes no position respecting the validity of any patent rights asserted in connection with any item mentioned in this standard. Users of this standard are expressly advised that determination of the validity of any such patent rights, and the risk of infringement of such rights, are entirely their own responsibility.

This standard is subject to revision at any time by the responsible technical committee and must be reviewed every five years and if not revised, either reapproved or withdrawn. Your comments are invited either for revision of this standard or for additional standards and should be addressed to ASTM International Headquarters. Your comments will receive careful consideration at a meeting of the responsible technical committee, which you may attend. If you feel that your comments have not received a fair hearing you should make your views known to the ASTM Committee on Standards, at the address shown below.

This standard is copyrighted by ASTM International, 100 Barr Harbor Drive, PO Box C700, West Conshohocken, PA 19428-2959, United States. Individual reprints (single or multiple copies) of this standard may be obtained by contacting ASTM at the above address or at 610-832-9585 (phone), 610-832-9555 (fax), or service@astm.org (e-mail); or through the ASTM website (www.astm.org). Permission rights to photocopy the standard may also be secured from the Copyright Clearance Center, 222 Rosewood Drive, Danvers, MA 01923, Tel: (978) 646-2600; <http://www.copyright.com/>